R → P

Podatki:

T	Y	X
A	846,72	501.86
B	933.43	439.25

Rezultat:

$d_{AB} = 106,95$

$\nu_A^B = 125^\circ 49' 56''$

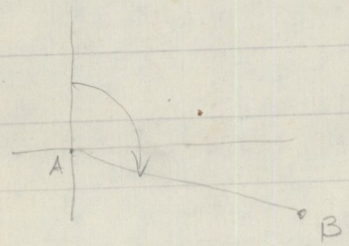
P → R

Podatki:

	Y	X
A	846,72	501.86
$d_{AB} = 106,95$	$\nu_A^B = 125^\circ 49' 56''$	

Rezultat:

T	Y	X
A	846,72	501.86
ΔY	86.71	ΔX -62.61
B	933.43	439.25



T I S K A N J E - PRINTER STAR NL-10

stisnjeni	(condensed)	:ALT X	Gostic Emil
mastni	(emphasized)	:ALT C	**Gostič Emil**
krepki	(strike)	:ALT V	~~Gostič Emil~~
podčrtano	(underline)	:ALT B	Gostič Emil
potenčni	(superscript)	:ALT M	Gostič ^{Emil}
indeksni	(subscript)	:ALT ,	Gostic $_{Emil}$
lepopisni	(NLQ)	:ALT .	Gostič Emil

Indexi(subscript) :H_2SO_4
potence(superscript) :$a^2-b^2=c^2$

Primeri kombiniranja posameznih načinov:

italic-podčrtan-potenca :*GOSTIC* ^{Emil}
-indeks- mastno :***Gostič*** $_{Emil}$

dvojno-podčrtano-(masten- index): GOSTIC $_{Emil}$

APF 5602

$X_B - X_A = MS \quad y_B - y_A = FX^2 + M_c^R F X^2 = \sqrt{X} \Rightarrow d$

$1/X * M_c^R = F \cos^{-1}$ ($y_B > y_A$) da → $\angle^{\circ\,dec}$ $F \to 0'' \Rightarrow \angle^{0'0''}$

ne $\boxed{+/- +360 =}$

AURORA

SCIENTIFIC calkulator

HC-687

KAVČIČ

AUTO POWEROFF MEMORI SAFE GUARD

STAT

POWER

2ndF DRG OFF ON

SIN1 COS1 tan1 TAB

hyp sin cos tan F↔E C

LRN ex 10x X→K1 CAD X→K2 nΣx n!

COMP ln Log K1 K2 CE

π x√y 3√ 1/x (x) HLT

EXP y^x √ x² ( )

→DMS

7 8 9 ÷ X→M

→DEG

4 5 6 X RM

1 2 3 − M+

0 +/− . + =

F → DMS

F DMS →

nepodporuje casio fx 17

casio fx 120

fx 220

fx 991

CANON F401

d ←

d °,'," →

CASIO fx-17 (stari ANS)

$X_B - X_A =$ ΔX^* zapišem z vsemi decimalkami. X^2 Mc M+

$Y_B - Y_A =$ X^2 M+

MR $\sqrt{\ }$ $\Rightarrow \underline{\underline{d}}$

1/x * ΔX^* = ARC COS $Y_B > Y_A$? da $\rightarrow$ $\underline{\underline{\nu}}^\circ = {}^\circ \times 60 = \underline{\underline{\nu}}'$

ne $\boxed{+/- +360 =}$ $- {}' \times 60 = \underline{\underline{\nu}}''$

preveriti!

$\nu_0^{\circ\,\prime\,\prime\prime}$ $\boxed{\circ\ \prime\ \prime\prime}$ Mc M+ sin * $d = \underline{\Delta Y} + Y_A = Y_B$

MR cos * $d = \underline{\Delta X} + X_A = X_B$

CASIO fx-68

$X_B - X_A = INV\ R{\to}P\,(Y_B - Y_A) = \underline{\underline{d}}$

$x \leftrightarrow y$ (?) ne → $\underline{\underline{\nu}}^{\circ dec}$ $INV\ {}^{\circ\,'\,''} \Rightarrow \underline{\underline{\nu}}^{\circ\,'\,''}$

da $\boxed{+360=}$

$d\ INV\ P{\to}R\ \nu^{\circ\,'\,''}\ \nu^{'\circ\,'\,''}\ \nu^{''\circ\,'\,''} = \Delta x\ Min$

$x \leftrightarrow y \Rightarrow \underline{\Delta y} + Y_A = \underline{\underline{Y_B}}$

$MR \Rightarrow \underline{\Delta x} + X_A = \underline{\underline{X_B}}$

CASIO fx-82A

$X_B - X_A = \text{INV } R \to P \left(Y_B - Y_A\right) = \Rightarrow d$

$X \leftrightarrow Y \ (+360 =) \ \underline{\underline{\nu}}^{\circ \text{dec}} \quad \text{INV } ^{\circ\,'\,''} \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

$d \text{ INV } P \to R \ \nu^{\circ\,'\,''} \ \nu^{'\circ\,'\,''} \ \nu^{''\circ\,'\,''} = \Delta X \text{ Min}$

$X \leftrightarrow Y \Rightarrow \underline{\underline{\Delta Y}} + Y_A = \underline{\underline{Y_B}}$

$MR \Rightarrow \underline{\underline{\Delta X}} + X_A = \underline{\underline{X_B}}$

CASIO fx-85M

$X_B - X_A = \text{INV } R \to P\ (Y_B - Y_A) = \underline{\underline{d}}$

$X \leftrightarrow Y\ (+360 =)\ \underline{\underline{\nu}}^{\circ}\ \text{INV}\ {}^{\circ\,\prime\,\prime\prime} \Rightarrow \underline{\underline{\underline{\nu}}}^{\circ\,\prime\,\prime\prime}$

$d\ \text{INV } P \to R\ \nu^{\circ\,\prime\,\prime\prime}\ \nu^{\prime\,\circ\,\prime\,\prime}\ \nu^{\prime\prime\,\circ\,\prime\,\prime} = \Delta X\ \text{Min}$

$X \rightleftarrows Y \Rightarrow \underline{\underline{\Delta Y}} + Y_A = \underline{\underline{Y_B}}$

$MR \Rightarrow \underline{\underline{\Delta X}} + X_A = \underline{\underline{X_B}}$

CASIO fx-100

$X_B - X_A = INV\ R \Rightarrow P\ (Y_B - Y_A) = \underline{\underline{d}}$

$x \leftrightarrow y\ (+360 =)\ \nu^{\circ}\ INV\ {}^{\circ}{}'{}'' \Rightarrow \underline{\underline{\nu^{\circ}{}'{}''}}$

$d\ INV\ P \Rightarrow R\ \nu^{\circ}{}^{\circ}{}'{}''\ \nu^{'}{}^{\circ}{}'{}''\ \nu^{''}{}^{\circ}{}'{}'' = \Delta X\ Min$

$x \leftrightarrow y \Rightarrow \underline{\Delta Y} + Y_A = \underline{\underline{Y_B}}$

$MR \Rightarrow \underline{\Delta X} + X_A = \underline{\underline{X_B}}$

CASIO fx - 115

$X_B - X_A = INV\ R \rightarrow P\ (Y_B - Y_A) = \underline{\underline{D}}$

$X \leftrightarrow Y\ (+360 =)\ \underline{\underline{\nu^{\circ}}}\ INV\ {}^{\circ\,'\,''} \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

$d\ INV\ P \rightarrow R\ \nu^{\circ}{}^{\circ\,'\,''}\ \nu^{'}{}^{\circ\,'\,''}\ \nu^{''}{}^{\circ\,'\,''} = \Delta X\ Min$

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

$MR \Rightarrow \Delta X + X_A = X_B$

CASIO fx-120

$X_B - X_A =$ INV R→P $(Y_B - Y_A) = \Rightarrow d$

$X \leftrightarrow Y$ $(+360 =) \Rightarrow Y^{odec}$ INV °'" $\Rightarrow Y^{°\,'\,''}$

CASIO fx-220

CASIO fx-250

$X_B - X_A =$ INV $R \to P\,(Y_B - Y_A) = \underline{\underline{d}}$

$X \leftrightarrow Y$ $(+360 =)$ $\underline{\underline{\nu^{\circ}}}$ INV $^{\circ\,'\,''} \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

d INV $P \to R$ $\nu^{\circ\,'\,''}\,\nu^{\circ\,'\,''}\,\nu^{\circ\,'\,''} = \Delta X$ Min

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

MR $\Rightarrow \Delta X + X_A = X_B$

CASIO fx-330

$X_B - X_A = \text{INV } R \to P \; (Y_B - Y_A) = \underline{\underline{d}}$

$X \leftrightarrow Y \; (+360 =) \; \nu^{\circ dec} \; \text{INV}^{\circ\,'\,''} \Rightarrow \nu^{\circ\,'\,''}$

$d \; \text{INV } P \to R \; {}^{\circ}\,{}^{\prime\prime\prime}\,{}^{\prime}\,{}^{\prime\prime}\,{}^{\circ}\,{}^{\prime}\,{}^{\prime\prime} = \Delta X \; \text{Min}$

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

$MR \Rightarrow \Delta X + X_A = X_B$

CASIO fx-350

$X_B - X_A = INV\ R\text{-}P\ (Y_B - Y_A) = \underline{\underline{d}}$

$X \leftrightarrow Y\ +360 = \nu^{\circ}\ INV\ {}^{\circ\,\prime\,\prime\prime} \Rightarrow \underline{\underline{\nu^{\circ\,\prime\,\prime\prime}}}$

$d\ INV\ P \rightarrow R\ \nu^{\circ\,\prime\,\prime\prime}\nu^{\prime\circ\,\prime\,\prime\prime}\nu^{\prime\prime\circ\,\prime\,\prime\prime} = \Delta X\ Min$

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

$MR \Rightarrow \Delta X + X_A = X_B$

CASIO fx-450

$X_B - X_A$ = SHIFT $R \to P$ $(Y_B - Y_A)$ = d

$x \leftrightarrow y$ (+360 =) $\nu^{\circ\,dec} \to {}^{\circ}{}'{}'' \Rightarrow \nu^{\circ\,'\,''}$

d SHIFT $P \to R$ $\underline{\nu}^{\circ\,'\,''}\,\underline{\nu}^{\circ\,'\,''}\,\nu^{\circ\,'\,''} = \Delta X$ Min

$x \leftrightarrow y \Rightarrow \Delta Y + Y_A = Y_B$

MR $\Rightarrow \Delta X + X_A = X_B$

CASIO fx-550

$X_B - X_A = INV\ R \to P\ (Y_B - Y_A) = \underline{\underline{d}}$

$X \rightleftarrows Y\ (+360 =) \Rightarrow \nu^{\circ\ dec}\quad INV\ {}^{\circ\,'\,''} \Rightarrow \nu^{\circ\,'\,''}$

$d\ INV\ P \to R\ \nu^{\circ\,'\,''}, \nu^{\circ\,'\,''}, \nu^{\circ\,'\,''} = \Delta X\ Min$

$X \leftrightarrow Y \Rightarrow \underline{\Delta Y} + Y_A = \underline{\underline{Y_B}}$

$MR \Rightarrow \underline{\Delta X} + X_A = \underline{\underline{X_B}}$

$= 560$

CASIO fx-991

$X_B - X_A = \text{INV } R \to P \, (Y_B - Y_A) = \underline{\underline{d}}$

$X \leftrightarrow Y \; (+360 =) \; \nu^{\circ} \; \text{INV } {}^{\circ}{}'{}'' \Rightarrow \underline{\underline{\nu^{\circ}{}'{}''}}$

CASIO fx 2500

(R·P)

$X_B - X_A = INV + (Y_B - Y_A) = \Rightarrow d$

$X \leftrightarrow Y \; (+360 =) \Rightarrow \underline{\underline{)^{\circ dec}}} \; INV \; {}^{\circ}{}'{}'' \Rightarrow \underline{\underline{)^{\circ}{}'{}''}}$

$d \; INV -)^{\circ\circ''}\,)^{\circ\circ''}\,)^{\circ\circ''} = \Delta X \; Min$

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

$MR \Rightarrow \Delta X + X_A = X_B$

CASIO fx-3200

$X_2 - X_1 =$ INV $R \to P\,(Y_2 - Y_1) = \underline{\underline{d}}$

$X \leftrightarrow Y$ $(+360=)$ $\nu^{\circ\,dec}$ INV $^{\circ\,\prime\,\prime\prime} \Rightarrow \nu^{\circ\,\prime\,\prime\prime}$

d INV $P \to R$ $^{\circ}\,01\,\prime\prime$ $'\,01\,\prime\prime$ $''\,01\,\prime\prime$ $=$ Min

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_1 = Y_2$

MR $\Rightarrow \Delta X + X_1 = X_2$

CASIO 3600P

$X_B - X_A = \text{INV } R \to P \, (Y_B - Y_A) = \Rightarrow \underline{\underline{d}}$

$X \leftrightarrow Y \; (+360 =) \; \underline{\nu}^{\circ dec} \quad \text{INV}^{\circ\,'\,''} \Rightarrow \underline{\underline{\underline{\nu}^{\circ\,'\,''}}}$

$d \; \text{INV } P \to R \; \nu^{\circ\,\circ\,'\,''} \; \nu^{'\circ\,'\,''} \nu^{''\circ\,'\,''} = \underline{\underline{\Delta X}} \; Min$

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = \underline{\underline{Y_B}}$

$MR \Rightarrow \Delta X + X_A = \underline{\underline{X_B}}$

CASIO FX 3800P

$X_B - X_A =$ INV R → P $(y_B - y_A) =$ ⇒ $\underline{\underline{d}}$

shift x → y (+360 =) ν ° dec [redacted] shift ° ' " ⇒ ν ° ' "

CASIO fx-7100

$X_B - X_A = \text{INV } R \to P(Y_B - Y_A) = \Rightarrow \underline{\underline{d}}$

$X \leftrightarrow Y\ [+360=] \Rightarrow \underline{\underline{)^{\circ dec}}}$ INV $^{\circ\,'\,''} \Rightarrow \underline{\underline{)^{\circ\,'\,''}}}$

d INV $P \to R$ $)^{\circ\,'\,''}$ $)^{'\circ\,'\,''}$ $)^{''\circ\,'\,''}$ $= \Delta X$ Min

$X \leftrightarrow Y \Rightarrow \underline{\Delta Y} + Y_A = \underline{\underline{Y_B}}$

MR $\Rightarrow \underline{\Delta X} + X_A = \underline{\underline{X_B}}$

ANS COMMODORE

MODEL
SR 4148 R

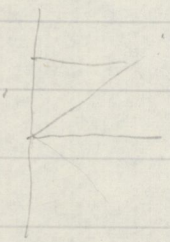
$Y_B - Y_A$ = STO 1

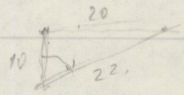
$X_B - X_A$ = X⇔Y RCL 1 → P ⇒ d

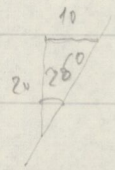
X⇔Y ⇒ $\nu^{\circ dec}$ − $^{\circ} \times 60 = \nu'$

− $' \times 60 = \nu''$

$\frac{180}{128}$







$(X_B - X_A)$ X⇔Y

~~d X⇔Y~~

~~ν°~~ $'' \div 60 + ' \div 60 + ^{\circ}$ = STO 1

d X⇔Y RCL 1 → R ⇒ ΔX ~~+ X_A = X_B~~ STO 2

~~RCL 1 ⇒ Δ~~

X⇔Y ⇒ $\Delta Y + Y_A = Y_B$

RCL 2 ⇒ $\Delta X + X_A = X_B$

CONCORDE 2

$Y_B - Y_A = STO$

$X_B - X_A = X^2 + MR\,X^2 = \overset{INV}{\sqrt{\ }} \Rightarrow \underline{\underline{d}}$

$1/x * MR = INV\,COS$ $\left(\frac{Y_B - Y_A}{2}\right)$ da $\rightarrow \underline{\underline{)'}}$ ° dec

ne $\boxed{+/- + 360 =}$

$- ° = \times 60 = \underline{\underline{)'}}$

$- ' = \times 60 = \underline{\underline{)''}}$

$)° +)' \div 60 +)'' \div 3600 = STO$

$sin * d = \Rightarrow \underline{\Delta Y} + Y_A = \underline{\underline{Y_B}}$

$MR\ cos * d = \Rightarrow \underline{\Delta X} + X_A = \underline{\underline{X_B}}$

ELORG ruski ANS

$X_B - X_A = Min \quad Y_B - Y_A = FX^2 + MR\,FX^2 = \sqrt{\ } \Rightarrow d$

$1/X \times MR = F\cos^{-1}$ $Y_B > Y_A$? $\rightarrow$ ν °dec

$\boxed{+/- +360 =}$

$\_° \times 60 = \underline{\nu'}$

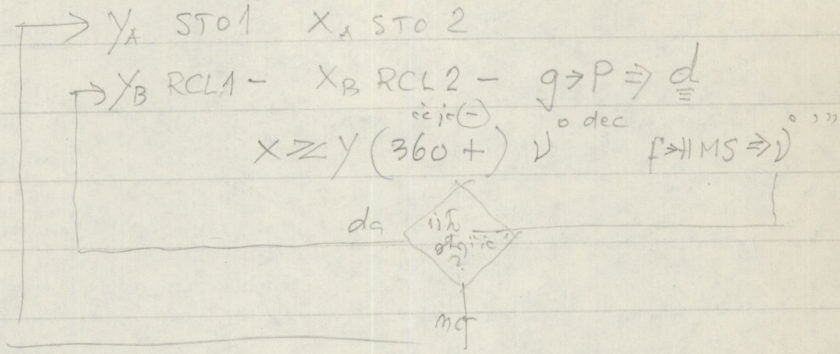
$\_' \times 60 = \underline{\nu''}$

$\nu.°'''$ $\boxed{° \; ' \; ''}$ Min

$\sin \times d = \Delta Y + Y_A = Y_B$

$MR \cos \times d = \Delta X + X_A = X_B$

HP 15



Y_A STO 1 X_A STO 2 d STO 3 ν° ' " STO Ø

ν d

RCL Ø g→H RCL 3 $\boxed{f \to R}$ ⇒ Δx RCL 2 + ⇒ Y_B

x⇄y ⇒ Δy RCL 1 + ⇒ Y_B

HP 28c

REAL → COMPLEX REAL → POLAR

Y_B ↑ Y_A − X_B ↑ X_A − SWAP R→C R→P

C→R 360 + HMS

	DISPLAY
Y_B 432.21 ENTER	1: 432.21 Y_B
Y_A 956.72 −	1: −524.51 (Y_B-Y_A)
	2: −524.51 (Y_B-Y_A)
X_B 721.45 ENTER	1: 721.45 X_B
	2: −524.51 (Y_B-Y_A)
X_A 316.17 −	1: 405.28 (X_B-X_A)
	2: 405.28 (X_B-X_A)
SWAP	1: −524.51 (Y_B-Y_A)
R → C	1: (405.28, −524.51)
R → P	1: (662.844, −52.307)
	2: 662.844
C → R	1: −52.307
	2: 662.844
360 +	1: 307.693
	2: 662.844
HMS	1: 307 41 33.5

PRIVILEG 1081 SR

$X_2 - X_1 = \text{INV } R \to P \; (Y_2 - Y_1) = \underline{\underline{d}}$

$x \leftrightarrow y \; (+360 =) \; \nu^{\circ dec} \; \text{INV} \; \vec{\circ}\,'\,'' \Rightarrow \nu^{\circ\,'\,''}$

$d \; \text{INV } P \to R \; \nu.^{\circ\,'\,''} \; \vec{\circ\,'\,''} \Rightarrow \Delta x \; MS$

$x \leftrightarrow y \Rightarrow \underline{\Delta y} + Y_1 = \underline{\underline{Y_2}}$

$M_c^R + X_1 = \underline{\underline{X_2}}$

PRIVILEG LC 1082 SR

$(X_B - X_A)$ INV $R \to P$ $(Y_B - Y_A) = \underline{\underline{d}}$

$X \leftrightarrow Y$ $(+360 =)$ $\underline{\underline{\nu}}^{\circ}$ INV $^{\circ\,'\,''} \Rightarrow \underline{\underline{\nu}}^{\circ\,'\,''}$

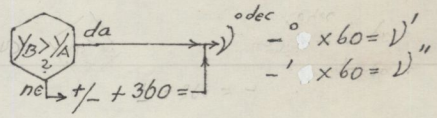
d INV $P \to R$ $\nu^{\circ\,'\,''}\ \nu'^{\circ\,'\,''}\ \nu''^{\circ\,'\,''} = Min$

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

$MR \Rightarrow \Delta X + X_A = X_B$

ROGER F 6 (ANS)

$X_B - X_A = mt \quad Y_B - Y_A = X^2 + mr \cdot X^2 = \sqrt{} \Rightarrow d$

$1/x * mr = \arccos$ 

$'' \div 60 + ' \div 60 + ° = mc\ mt$

$\sin * d = \Delta Y + Y_A = Y_B$

$mr \cos * d = \Delta X + X_A = X_B$

Slika

SHARP

EL - 506

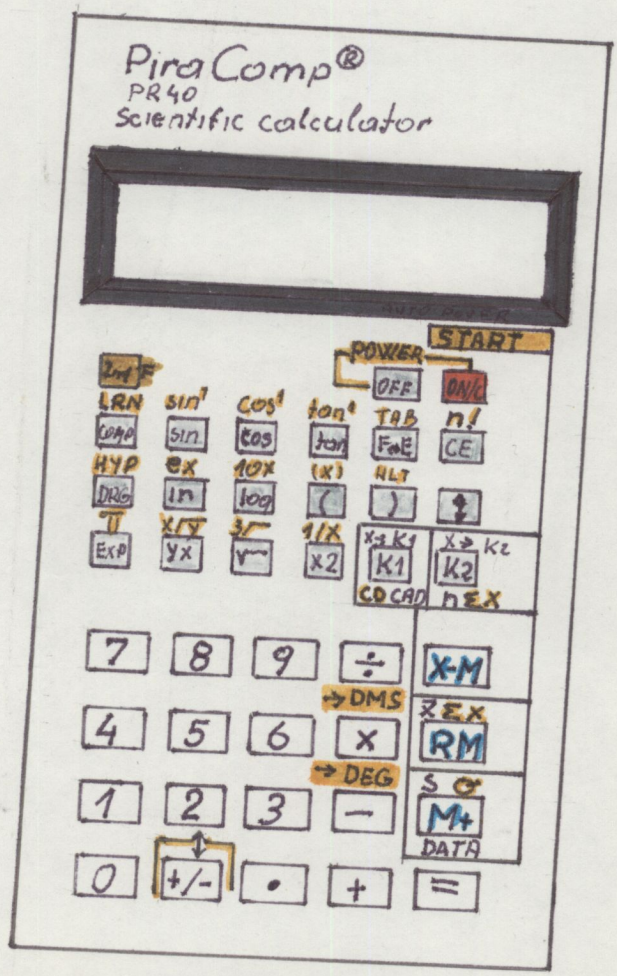
$Y_B - Y_A = X \rightarrow M$

$X_B - X_A = \updownarrow RM \xrightarrow{2nd\,F} r\theta \Rightarrow d$

$\updownarrow (+360=) \Rightarrow \underline{V}^{\circ dec} \quad DMS \xrightarrow{2nd\,F} \underline{\underline{V}}^{\circ\,'\,''}$

MURK

glej ER 92



ELECTRONIC CALCULATOR

EL 506-H

LCD & IC ARE MADE IN JAPAN

$y_B - y_A = x \rightarrow M$

pej SHARP EL 545H
SHARP EL 506P
SHARP EL 565

10-DIGIT SCINTIFIC CALCULATOR

AUTO POWER OFF

2nd F	DRG (DRG)			OFF	DN/C
hyp	sin	cos	tan	F↔E	CE
DEG	in	log	a (→n θ)	b (→x,y)	↔
EXP	yx	√	x^2	(	)
	7	8	9	÷	X-M
	4	5	6	X	RM
	1	2	3	−	M+
	0	+/−	•	+	=

Mätač

EL-506H LC 616 (JUG)

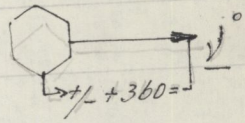
COMPONENT MADE IN JAPAN

K_1 K_2

$X_B - X_A = X \rightarrow M$

$Y_B - Y_A = X^2 + RM\ x^2 = \sqrt{\ } \Rightarrow d$

2nd F
$1/X$ * RM = 2nd F $\cos^{-1}$



$\angle$ ° dec 2nd F DMS ⇒ ° ' "

$\angle$ ° ' " 2nd F → DEG $X \rightarrow M$

$\sin * d = \Delta y + Y_A = Y_B$

$RM \cos * d = \Delta X + X_A = X_B$

EL - 506P

(HANDL-BÜROMASCHINEN)

$Y_B - Y_A = X \rightarrow M$

$X_B - X_A = X \leftrightarrow Y \quad RM \xrightarrow{2nd\,F} R\Theta \Rightarrow d$

$\Rightarrow y^{\circ\,\prime\,\prime\prime}$ (°dec 2nd F)

10-DIGIT SCIENTIFIC CALCULATOR

Žganec Ivon

glej
SAARPEL 545H
-"- 306P
-"- 566

2nd F	DRG				
~~arc hyp~~ hyp	SIN⁻¹ SIN	tan⁻¹ COS	TAB tan	TAB F↔E	π CE
DMS →DEG	e^x E IN	10^x F LOG	−π e a	→xy b	CPLX ↔
π A e^x P	x↔y B y^x	√ C √	1/x x²	↕ (	n Σx)
7	8	9	BIN ÷		Σx² XM
4	5	6	OCT ×		RM
1	2	3	xEx −		DATA CD M+
0	+/−	RND .	DEC +	AC	% =

Y_B

X_B

SHARP

EL - 506 H

$Y_B - Y_A = X \rightarrow M$

$X_B - X_A = \updownarrow$ RM $\xrightarrow{2nd\,F} \rightarrow r\Theta \rightarrow \underline{\underline{d}}$

$\updownarrow (+360 =) \Rightarrow \nu^{\circ}$ oder $\xrightarrow{2nd\,F} \rightarrow DMS \Rightarrow \underline{\underline{\nu^{\circ\,\prime\,\prime}}}$

gleich Tudi SHARP 506P

SHARP EL-545H

10 DIGIT

als T-W Rechner 501 56 Funk.

$Y_B - Y_A = \boxed{X \rightarrow M_1}$

$X_B - X_A = a \quad RM_1 \quad b \overset{2ndF}{\rightarrow} r\theta \Rightarrow \underline{\underline{d}}$

$b \Rightarrow \nu^{\circ\,dec} (+360 =) \overset{2ndF}{\rightarrow} DMS \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

$d \quad \underline{a} \quad \nu^{\circ\,'\,''} \rightarrow DEG \quad \underline{b} \overset{2ndF}{\rightarrow} xy \Rightarrow \Delta X \quad X \rightarrow M_1$

$b \Rightarrow \Delta Y + Y_A = Y_B$

$MR \Rightarrow \Delta X + X_A = X_B$

SHARP EL 506 P

$Y_B - Y_A = X \rightarrow M$

$X_B - X_A = a \; RM \; b \xrightarrow{2ndF} \rightarrow r\theta \Rightarrow \underline{d}$

$b \underset{(+360=)}{\Rightarrow} \nu^{\circ\,dec} \xrightarrow{2ndF} \rightarrow DMS \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

$d \; \underline{a} \; \nu^{\circ\,'\,''} \rightarrow DEG \; b \xrightarrow{2ndF} \rightarrow xy \Rightarrow \Delta x \quad x \rightarrow M$

$x \Leftrightarrow y \Rightarrow \Delta y + Y_A = Y_B$

$RM \Rightarrow \Delta x + X_A = X_B$

SHARP EL-508S

$X_B - X_A = STO \quad Y_B - Y_A = X^2 + RM\,x^2 = \sqrt{X} \Rightarrow \underline{\underline{d}}$

$1/x * RM = INV\ COS$ ($Y_B > Y_A$?) $\xrightarrow{da} \underline{\underline{\nu}}^{\circ} - {}^{\circ} = \times 60 = \underline{\underline{\nu}}' - {}' = \times 60 = \underline{\underline{\nu}}''$

$\xrightarrow{ne} \boxed{+/- + 360 =} \rightarrow$

$\nu^{\circ} + \nu' \div 60 + \nu'' : 3600 = X \rightarrow M$

$\sin * d = \Delta y + Y_A = Y_B$

$RM\ \cos \times d = \Delta X + X_A - X_B$

SHARP EL-509A

SHARP 510s

SHARP 512

$Y_2 - Y_1 = X \rightarrow M$

$(X_2 - X_1) \overset{2nd F}{\updownarrow} RM \xrightarrow{2nd F} \rightarrow \theta \Rightarrow \underline{\underline{d}}$

$\overset{2nd F}{\updownarrow} (+360 =) \Rightarrow \underline{\underline{\nu^{\circ dec}}} \xrightarrow{2nd F} \rightarrow DMS \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

$d \overset{2nd F}{\updownarrow} \nu^{\circ\,'\,''} \rightarrow DEG \xrightarrow{2nd F} \rightarrow XY \Rightarrow \Delta X \quad X \rightarrow M$

$\overset{2nd F}{\updownarrow} \Rightarrow \Delta Y + Y_A = Y_B$

$RM \Rightarrow \Delta X + X_A = X_B$

SHARP EL-531

$X_B - X_A = X \to M$

$Y_B - Y_A = X^2 + RM\,X^2 = \overset{2nd\,F}{\sqrt{X}} \Rightarrow \underline{\underline{d}}$

$\overset{2nd\,F}{1/X} * RM = \overset{2nd\,F}{COS}$ $(Y_B > Y_A)$ da $\to \underline{\underline{\nu}}$ $^{o\,dec}$ $- ^{o} = \times 60 = \underline{\underline{\nu}}'$

ne $\to$ +/- +360 = $\quad - ' = \times 60 = \underline{\underline{\nu}}''$

$^{o} + ' \div 60 + '' \div 3600 = X \to M$

$\sin \times d = \Rightarrow \underline{\Delta Y} + Y_A = \underline{\underline{Y_B}}$

$RM \cos \times d = \Rightarrow \underline{\Delta X} + X_A = \underline{\underline{X_B}}$

SHARP - EL-531P

$y_B - y_A = X \rightarrow M$

$(x_B - x_A)$ 2ndF $x \leftrightarrow y$ RM 2ndF $\rightarrow r\theta \Rightarrow d$

2ndF $x \leftrightarrow y$ [če je − +360 =] $\Rightarrow$) ° dec °M'S" $\Rightarrow$) ° ' "

$\boxed{\text{DRG}}$ (DEG)

) ° ' " 2ndF DRG = 2ndF $x \leftrightarrow y$ d

2ndF $x \leftrightarrow y$ 2ndF $\rightarrow xy \Rightarrow (x)$

2ndF $x \leftrightarrow y \Rightarrow (y)$

SHARP EL 540

$Y_B - Y_A = X \rightarrow M$

$X_B - X_A = X^2 + RM\,X^2 = \sqrt{\ } \Rightarrow \underline{d}$

$1/x * RM = \overset{2nd\,F}{\cos^{-1}}$ $\quad Y_B \underset{?}{>} Y_A$ $\qquad y^{\circ}\,dec \rightarrow DMS \Rightarrow y^{\circ\,'\,''}$

$+/- + 360 =$

$y^{\circ\,'\,''} \rightarrow DEG \quad X \rightarrow M$

$\sin x \; d = \Delta y + Y_A = Y_B$

$RM \cos x \; d = \Delta x + \Delta A = X_B$

SHARP EL-556

$Y_B - Y_A = X \to M \quad X_B - X_A = \boxed{a}\ RM\ \boxed{b} \to r\Theta \Rightarrow \underline{\underline{d}}$

$\boxed{b} \Rightarrow \nu^{\circ\ dec}$

$d \quad \underline{a} \quad \nu^{\circ\ '\ ''} \to DEG \quad b \Rightarrow \overset{2ndF}{XY} \Rightarrow \Delta X \quad X \to M_1$

$b \Rightarrow 63.180 + 200 = \underline{\underline{Y_B}}$

$MR \Rightarrow \Delta X + X_A = \underline{\underline{X_B}}$

SHARP PC - 1401

$Y_B - Y_A = X \rightarrow M \; (X_B - X_A) \updownarrow$ RM SHIFT $\rightarrow r\Theta \Rightarrow \underline{\underline{d}}$

$\updownarrow$ (+360 =) $\Rightarrow \underline{\underline{\nu^{\circ}}}$ SHIFT $\rightarrow$ DMS $\Rightarrow \underline{\underline{\underline{\nu^{\circ\,'\,''}}}}$

$\nu^{\circ\,'\,''} \rightarrow$ DEG $\updownarrow$ d $\updownarrow$ SHIFT $\rightarrow$ XY $\Rightarrow \Delta X$ $X \rightarrow M$

$\updownarrow \Rightarrow \Delta Y + Y_A = Y_B$

RM $\Rightarrow \Delta X + X_A = X_B$

SHARP 1430

SHARP 5103s

$(X_n - X_s) \rightarrow POL\ (Y_n - Y_s) = \Rightarrow \underline{\underline{d}}$

$RCL\ E \Rightarrow [+360=]\ \underline{\underline{\nu^{\circ dec}}}\ \ 2^{nd}F \rightarrow DMS\ \ \underline{\underline{\nu^{\circ\,'\,''}}}$

---

več kotov z enega stojišča

X_s STO A $\qquad Y_s$ STO B

$(X_1 - RCL\,A) \rightarrow POL\ (Y_1 - RCL\,B) = \underline{\underline{d}}$

$RCL\ E\ (+360=) \Rightarrow \underline{\underline{\nu^{\circ dec}}} \rightarrow 2^{nd}F \rightarrow DMS \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

da — ISTO STOJIŠČE? — ne

ali

Y_A STO A

$Y_B - RCL\,A =$ STO C $\qquad X_B - RCL\,B =$ STO D

$2^{nd}F\ D \rightarrow POL\ 2^{nd}F\ C = \underline{\underline{d}}$ $\qquad RCL\ E\ (+360=) \Rightarrow \nu^{\circ dec}$

$2^{nd}F \rightarrow DMS \Rightarrow \nu^{\circ\,'\,''}$

$d\ \ {}^{2nd F}_{REC}\ \nu^{\circ\,'\,''} \rightarrow DEG = \Delta X$ STO M

$RCL\ E \Rightarrow \Delta Y + Y_A = Y_B$

$RCL\ M \Rightarrow \Delta X + X_A = X_B$

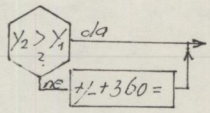
./.

SHARP EL 5813

$X_2 - X_1 = X \rightarrow M$

$Y_2 - Y_1 = X^2 + RMX^2 = \sqrt{\ } \Rightarrow d$

$1/x * RM = \overset{2ndF}{\cos^{-1}}$



ν^{odec} $- ^{\circ} = \times 60 = \underline{\underline{\nu}}'$

$- ' = \times 60 = \underline{\underline{\nu}}''$

nima DMS

$\nu^{\circ\,'\,''}$ $\overset{2ndF}{DEG}$ $X \rightarrow M$

$\sin \times d = \Delta y + Y_1 = Y_2$

$RM \cos \times d = \Delta X + X_1 = X_2$

TI 30 GALAXY

$Y_B - Y_A$ = STO $(X_B - X_A)$ x⇄y RCL INV P→R x⇄y ⇒ $\underline{\underline{d}}$

x ⇄ y) $\overset{\circ\,dec}{\downarrow}$ INV DMS-DD ⇒ $\underline{\underline{)\,^{\circ}\,'\,''}}$

(+360 =)

d x⇄y)°'" DMS-DD P→R ⇒ Δy STO

x⇄y ⇒ $\underline{\Delta x} + X_A = \underline{\underline{X_B}}$

RCL ⇒ $\underline{\Delta y} + Y_A = \underline{\underline{Y_B}}$

TI 30 LCD

$X_B - X_A = STO \quad Y_B - Y_A = X^2 + RCL\ X^2 = \sqrt{x} \Rightarrow \underline{\underline{d}}$

$1/x * RCL = INV\ COS\ \langle Y_B > Y_A \rangle$ ne $\boxed{+/- +360 =}$ $\rightarrow \nu^\circ$ dec

$- {}^\circ = \times 60 = \underline{\nu'}$

$- {}' = \times 60 = \underline{\nu''}$

$Y_B = Y_A + d \sin \nu_A^B$

$X_B = X_A + d \cos \nu_A^B$

$\nu^\circ + \nu' \div 60 + \nu'' \div 3600 = STO$

$\sin \times d = \underline{\Delta Y} + Y_A = \underline{\underline{Y_B}}$

$RCL\ \cos \times d = \underline{\Delta X} + X_A = \underline{\underline{X_B}}$

TI 31 SOLAR

$Y_B - Y_A$ = STO

$(X_B - X_A)$ $\overset{INV}{X \gtrless Y}$ RCL INV $R \to P \Rightarrow \nu^{\circ dec}$

$\overset{INV}{X \gtrless Y} \Rightarrow \underline{\underline{d}}$ zapíšem

$\overset{INV}{X \gtrless Y} \Rightarrow \nu^{\circ dec}$ (+ 360 =) $\overset{2nd}{DMS \to DD} \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

d $\overset{2nd}{X \gtrless Y}$ $\nu^{\circ\,'\,''}$ $\overset{2nd}{DMS\text{-}DD}$ $\overset{2nd}{P \to R} \Rightarrow \Delta Y$ STO

$\overset{2nd}{X \gtrless Y} \Rightarrow \Delta X + X_A = X_B$

RCL $\Rightarrow \Delta Y + Y_A = Y_B$

TI 33

Po potrebi M_1 ON/C (brišem spomin M_1)

(1)

$X_b - X_A = M_1+ \quad Y_B - Y_A = X^2 + M1 = X^2 = \sqrt{X} \Rightarrow d$

$1/x * M_1 = = INV\ COS$ ($Y_B > Y_A$?) → $\nu^{\circ dec}$ $- ^\circ = \times 60 = \nu'$ $- ' = \times 60 = \nu''$

ne → $\boxed{+/- +360 =}$

(2) Iz enega stojišča računam več dolžin in smer. Rotor

→ Po potrebi brišem spomine $\boxed{M_1\ ON/C,\ M_2\ ON/C,\ M_3\ ON/C}$

$X_A\ M_1+ \qquad Y_A\ M_2+$

$X_B - M_1 = = M_3+ \quad Y_B - M_2 = = X^2 + M_3 = X^2 = \sqrt{X} \Rightarrow d$

$1/x * M_3 = = INV\ COS$ ($Y_B > Y_A$?) → $\nu^{\circ dec}$ $- \nu^\circ = \times 60 = \nu'$ $- \nu' = \times 60 = \nu''$

ne → $\boxed{+/- +360 =}$

da → (ISTO STOJIŠČE?)

ne

$^\circ + ' \div 60 + '' \div 3600 = M_1+ \quad d\ M_2+$

$M_1 = sin * M_2 = = \Delta Y + Y_A = Y_B$

$M_1 = COS * M_2 = = \Delta X + X_A = X_B$

TI 45

$X_B - X_A$ = STO $Y_B - Y_A$ = x^2 + RCL x^2 = $\sqrt{x}$ ⇒ $\underline{\underline{d}}$

1/x × RCL = INV COS ($Y_B > Y_A$) ——— ν° − ° = × 60 = $\underline{\nu'}$

+/− + 360 = ——— ≡ − ' = × 60 = $\underline{\underline{\nu''}}$

TI SR-50A

$y_B - y_A = STO$

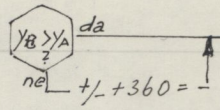
$x_B - x_A = x^2 + RCL\ x^2 = \sqrt{x} \Rightarrow d$

$1/x * RCL =$ arc cos $(y_B > y_A)$ → ν° $- {}^{\circ} = \times 60 = \nu'$

ne $+/- + 360 =$ $- {}' = \times 60 = \nu''$

TI-53

$X_B - X_A = STO \quad Y_B - Y_A = X^2 + RCL\,X^2 = \sqrt{x} \Rightarrow \underline{\underline{d}}$

$1/x * RCL = INV\ COS$ 

$\underline{\underline{\nu}}^\circ - {}^\circ = \times 60 = \underline{\underline{\nu}}'$

$- {}' = \times 60 = \underline{\underline{\nu}}''$

$Y_B = Y_A + d \sin \underline{\nu}$

$X_B = X_A + d \cos \nu$

$\nu^\circ + \nu' \div 60 + \nu'' \div 3600 = STO$

$sin * d = \Delta y + Y_A = \underline{\underline{Y_B}}$

$RCL\ cos * d = \Delta x + X_A = \underline{\underline{X_B}}$

UNIS SLR T-85

$X_B - X_A = STO \quad Y_B - Y_A = X^2 + RCL \quad X^2 = \sqrt{X} \Rightarrow \underline{\underline{d}}$

$1/x * RCL = INV\ COS$ $\langle Y_B > Y_A \rangle$ $\xrightarrow{}$ $\underline{\underline{\nu}}^{\circ\,dec}$ $- {}^{\circ} = \times 60 = \underline{\underline{\nu}}'$

$\xrightarrow{?}$ $\boxed{+/- +360 =}$ $- {}' = \times 60 = \underline{\underline{\nu}}''$

$\nu^{\circ} + \nu'/60 + \nu''/3600 = STO$

$sin * d = \Delta y + Y_A = Y_B$

$RCL\ cos * d = \Delta x + X_A = X_B$

LOGITACH LC-604

$X_B - X_A = STO \quad Y_B - Y_A = X^2 + RCL\ x^2 = \sqrt{x} \Rightarrow \underline{\underline{d}}$

$1/x \times RCL = arc\ cos$ $\langle Y_B > Y_A \rangle$ da $\rightarrow$ ν° dec $\quad - ^{\circ} = \times 60 = \nu'$

2 $\quad - ' = \times 60 = \nu''$

$\boxed{rcl \quad +/- + 360 =}$

$\nu^{\circ} + \nu' \div 60 + \nu'' \div 3600 = STO$

$sin \times d = \Delta y + Y_A = Y_B$

$RCL\ cos \times d = \Delta x + X_A = X_B$

Logitach

$X_n - X_s = x \rightarrow M \qquad y_n - y_s = x^2 + RM\,x^2 = \sqrt{\ } \Rightarrow \underline{\underline{d}}$

$F\ 1/x \times RM = F\cos^{-1}$ $\boxed{y_n > y_s\ ?}$ da $\longrightarrow$ $)^{\circ}$ dec $\rightarrow F \rightarrow DMS \Rightarrow)^{\circ\ '\ ''}$

ne $+/- +360 =$

MBO ALPHA 802

$Y_B - Y_A = X \rightarrow M$

$X_B - X_A = X \leftrightarrow Y \quad RM \quad F \rightarrow r\theta \Rightarrow d$

$X \leftrightarrow Y \; (+360 =) \; \nu^{\circ\,dec} \quad F \rightarrow DMS \Rightarrow \nu^{\circ\,\prime\,\prime\prime}$

$d \quad X \leftrightarrow Y \quad \nu^{\circ\,\prime\,\prime\prime} \rightarrow DEG. \quad F \rightarrow XY \Rightarrow \Delta X \quad X \rightarrow M$

$X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

$RM \Rightarrow \Delta X + X_A = X_B$

MR 610 (IMP-Lüdy:)

$(X_B - X_A) + (Y_B - Y_A) \rightarrow r\alpha \Rightarrow \underline{\underline{d}}$

$x \leftrightarrow y \; (+360 =) \; \underline{\Rightarrow \nu^{\circ dec}} \; FDMS \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

$d + \nu^{\circ\,'\,''} \; DEG \; F \rightarrow xy \Rightarrow \Delta x \quad x \rightarrow M$

$x \leftrightarrow y \Rightarrow \underline{\underline{\Delta y}} + Y_A = \underline{\underline{Y_B}}$

$MR \Rightarrow \underline{\underline{\Delta x}} + X_A = \underline{\underline{X_B}}$

Night and Day

$Y_B - Y_A = X \rightarrow M$

$(X_B - X_A) \overset{2nd\,F}{\updownarrow} MR \overset{2nd\,F}{\rightarrow} r\theta \Rightarrow d$

$\overset{2nd\,F}{\updownarrow} (+360 =) \nu^{\circ\,dec} \overset{2nd\,F}{\rightarrow} DMS \Rightarrow \nu_A^B$

$\nu^{\circ\,'\,''} \overset{2nd\,F}{\rightarrow} DEG$ $X \rightarrow M$

upotreba $\Rightarrow X\,Y$! ne pc $d \cdot \sin$ $d \cdot \cos x$

MR $\sin x$

ZAGAR
3D

OLYMPIA LCD 380

$X_B - X_A = Min\ (Y_B - Y_A)\ x^2 + RM\ x^2 = \sqrt{\ } \Rightarrow \underline{d}$

$1/x * RM = ARC\ COS$ ⟨$Y_B > Y_A$⟩ da →)° dec DMS ⇒)° ' "

ne → $\boxed{\pm +360 =}$

PANASONIC

$X_B - X_A = INV\ R \to P\ (y_B - y_A) = \underline{\underline{d}}$

$X \leftrightarrow y\ (+360 =)\ \nu^{\circ\,dec}\ F \to DMS \Rightarrow \underline{\underline{\nu^{\circ\,\prime\,\prime\prime}}}$

$d\ INV\ P \to R\ \nu^{\circ\,\prime\,\prime\prime}\ F\ DMS \to = \Delta X\ \ X \to M$

$X \leftrightarrow y \Rightarrow \underline{\underline{\Delta y}} + y_A = \underline{\underline{y_B}}$

$M_{RC} \Rightarrow \underline{\underline{\Delta X}} + X_A = \underline{\underline{X_B}}$

PHILIPS SBC 1704

$X_B - X_A = STO \quad Y_B - Y_A = x^2 + MR \quad x^2 = \sqrt{} \Rightarrow d$

$1/x * MR = F\cos^{-1}$ $\boxed{Y_B > Y_A ?}$ da $\longrightarrow$ ν° dec

nc $\rightarrow$ $\boxed{+/- + 360 =}$

$- {}^{\circ} = * 60 = \nu'$

$- {}' = \times 60 = \nu''$

${}^{\circ} + {}' \div 60 + {}'' \div 3600 = STO$

$\sin * d = \Rightarrow \Delta Y + Y_A = Y_B$

$RCL \cos \times d = \Rightarrow \Delta x + X_A = X_B$

PHILIPS SBC 1745

$Y_B - Y_A$ = STO 1 $(X_B - X_A)$ x ↔ y RCL 1 → POL ⇒ $\underline{\underline{d}}$

x ↔ y (+360 =) $\underline{\underline{\nu^\circ}}$ DMS ⇒ $\underline{\underline{\nu^{\circ\,'\,''}}}$

d F x ↔ y $\nu^{\circ\,'\,''}$ → DEG F → REC ⇒ Δx STO 1

F x ↔ y ⇒ Δy + Y_A = Y_B

RCL 1 ⇒ Δx + X_A = X_B

PRIVILEG 585 D-E-NC

$X_B - X_A = X - M \quad Y_B - Y_A = X^2 + MR\,X^2 = \sqrt{\ } \Rightarrow \underline{d}$

$1/x * MR = ARC\ COS$ $\boxed{Y_B \overset{?}{>} Y_A}$ $\xrightarrow{da}$ $\nu^{\circ\,dec}$ $- {}^\circ \times 60 = \underline{\underline{\nu'}}$

ne $\boxed{+\angle + 360 =}$ $- {}' \times 60 = \underline{\underline{\nu''}}$

$'' \div 60 + ' \div 60 + {}^\circ = \Rightarrow \nu^{\circ\,dec} \quad x - M$

$\sin x \quad d = \Delta y + Y_A = Y_B$

$MR \cos x \quad d = \Delta x + X_A = X_B$

PRIVILEG-LC-814 PR

$Y_B - Y_A$ = STO 1 $X_B - X_A$ = INV $X \leftrightarrow Y$ RCL 1 $R \to P \Rightarrow d$

INV $X \leftrightarrow Y$ (+360 =) $\underline{V}^{\circ dec}$ INV $\to {}^{\circ}{}'{}''$ $\Rightarrow \underline{\underline{V}}^{\circ\,'\,''}$

$V.^{\circ\,'\,''}$ INV $\cancel{\circ\,'\,''} \to$ INV $X \leftrightarrow Y$ INV $P \to R \Rightarrow \Delta X$

d INV $X \leftrightarrow Y$ $V.^{\circ\,'\,''}$ $\boxed{\circ\,'\,'' \to}$ INV $P \to R \Rightarrow \Delta X$ STO 1

INV $X \leftrightarrow Y \Rightarrow \Delta Y + Y_A = Y_B$

RCL 1 $\Rightarrow \Delta X + X_A = X_B$

Privileg Lc 1021 SR

$X_B - X_A = MS \quad Y_B - Y_A = X^2 + MR\,X^2 = \sqrt{X} \Rightarrow \underline{\underline{d}}$

$1/X * MR = \arccos$ ($Y_B > Y_A$?) $\longrightarrow \nu^{\circ}$ oder $\rightarrow 0'''' \Rightarrow \underline{\underline{\nu^{\circ\,'\,''}}}$

$\rightarrow \boxed{+\angle + 360 =} \rightarrow \nu^{\circ}$

PRIVILEG LC 1070 SR

$X_B - X_A =$ ~~STO~~ MS $\quad Y_B - Y_A = X^2 + RCL\ X^2 = \sqrt{X} \Rightarrow \underline{\underline{d}}$

$1/X * $ ~~RCL~~ MR $= ARC\ COS\ (Y_B > Y_A)^2 \longrightarrow \underline{\underline{\nu}}^{\circ\ dec} \rightarrow {}^{\circ}\ {}'\ {}'' \ \underline{\underline{\underline{\nu}}}^{\circ\ '\ ''}$

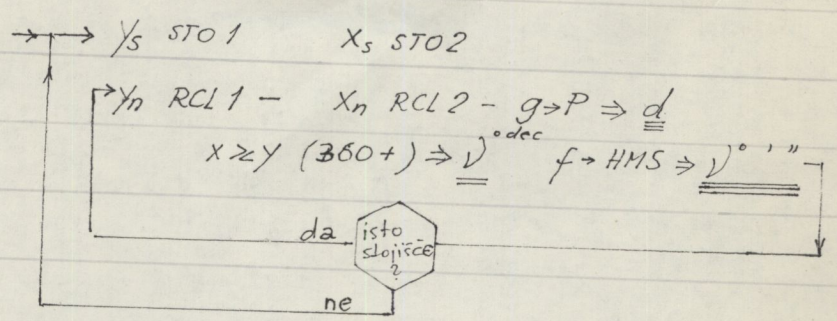
$+/- +360 =$

$^{\circ}\ '\ ''\ \ {}^{\circ}\ '\ '' \rightarrow$ ~~STO~~ MS

$\sin \times d = \Delta Y + Y_A = Y_B$

MR $\cos \times d = \Delta X + X_A = X_B$

HP 34c


Ys STO 1
Xs STO 2
Yn RCL 1 –
Xn RCL 2 –
g→P ⇒ d
x≷y (360+) ⇒ ν°dec
f→HMS ⇒ ν° ' "
da
isto stojišče ?
ne

$R \rightarrow P$

$P \rightarrow R$

PODATKI:

PRIMER: $\Delta y = -132$
$\Delta x = 67$

Rezultat: $d = 148.03$
$\nu^{dec} = -63.08876 + 360 = 296.9112$
$\nu^{\circ\prime\prime} = 296^\circ 54' 40''$

PRIMER:

T	y	x	d	ν_s^{m}
S	452	103		
1	600	159	158.24	69
2	500	39	80.00	
3	298	50	162,86	
4	320	170	148.03	

HP 25

Δy [↑] Δx [g→P] ⇒ d [x⇄y] ⇒ ν^{dec} [f→HMS]

$\nu^{\circ\prime\prime}$ [g→H] d [f→R] ⇒ Δx [x⇄y] Δy

CITIZEN SR II

Δy [x/y] Δx [F / R→P] ⇒ d [x/y] ⇒ ν^{dec} ⇒ [F / DMS]

$\nu^{\circ\prime\prime}$ [DMS→] [x/y] d [P→R] ⇒ Δx [x⇄y] Δy

COMPEX 8601

Δy [INV / R→P] Δx [=] d [x↔y] ⇒ ν^{dec} [INV / ° ′ ″]

d [INV / P→R] $\nu^{\circ\prime\prime}$ [° ′ ″ →] [=] Δx [x↔y] Δy

Underwood

Δy [x↔y] Δx [F / R→P] ⇒ d [x↔y] ⇒ ν^{dec} [F / DMS]

$\nu^{\circ\prime\prime}$ [DEG] [x↔y] d [P→R] ⇒ Δx [x→y] Δy

MBO MONARCH

Δy [x/y] Δx [r-p] ⇒ ν^{dec} [DMS] [x/y] ⇒ d

d [x/y] $\nu^{\circ\prime\prime}$ [deg] [p→r] ⇒ Δx [x/y] Δy

MBO 2000

Δy [x/y] Δx [R-P] ⇒ ν^{dec} [DMS] [x/y] ⇒ d

d [x/y] $\nu^{\circ\prime\prime}$ [DEG] [P→R] ⇒ Δx [x/y] Δy

MBO 3000

Δy [x/y] Δx [F / R▸P] ⇒ d [x/y] ⇒ ν^{dec} [F / DMS]

$\nu^{\circ\prime\prime}$ [DEG] [x/y] d [P→R] ⇒ Δx [x/y] Δy

MBO 4000 glej drugi list!

R → P

Podatki: $\Delta x = 67$
$\Delta y = -132$

REZULTAT: $d = 148.03$
$\nu^\circ = 296^\circ 54' 40''$

P → R

Podatki:

T	y	x
S	452	103
1	600	159
2	500	39
3	298	50
4	320	170

REZULTAT:

$d_1 = 158.24$	$\nu_S^1 = 69^\circ 16' 28''$
$d_2 = 80.00$	$\nu_S^2 = 143\ 07\ 48$
$d_3 = 162.86$	$\nu_S^3 = 251\ 00\ 32$
$d_4 = 148.03$	$\nu_S^4 = 296\ 54\ 40$

TI 51-III

Δx [x⇄y] Δy [INV 2nd P→R] ⇒ ν^{dec} [x⇄y] ⇒ d [x⇄y] ⇒ ν^{dec} (INV 2nd DMS-DD)

d [x⇄y] $\nu^{\circ\,'\,''}$ [2nd DMS-DD] [2nd P→R] ⇒ Δy [x⇄y] ⇒ Δx

TI 57-PROGR.

Δx [x⇄t] Δy [INV 2nd P→R] ⇒ ν^{dec} [x⇄y] ⇒ d (INV 2nd D.MS)

d [x⇄t] $\nu^{\circ\,'\,''}$ [2nd D.MS] [2nd P→R] ⇒ Δy [x⇄t] ⇒ Δx

TI 56 SR

CASIO 80, 330, 2600, 8000, 120

Δx [INV R→P] Δy [=] d [x⇄y] ν^{dec} (INV ←)

d [INV P→R] ν° [STO] ν' [STO] ν'' [STO] [=] ⇒ Δx [x⇄y] ⇒ Δy

CASIO 17, 21, 102

Δx [ARC +] Δy [=] d (mima x⇄y !!!) (mima ←)

d [ARC −] ν° [STO] ν' [STO] ν'' [STO] [=] ⇒ Δx

CASIO 31, 105

Δx [INV +] Δy [=] d (mima x⇄y !!!)

d [INV −] ν° [STO] ν' [STO] ν'' [STO] [=] ⇒ Δx

CASIO 81, 39, 2500

Δx [INV +] Δy [=] d [x⇄y] ν^{dec} (INV ←)

d [INV −] ν° [STO] ν' [STO] ν'' [STO] [=] ⇒ Δx [x⇄y] ⇒ Δy

LC-Y1

Δx [INV R→P] Δy [=] d [x⇄y] ν^{dec} [→DMS]

d [INV P→R] $\nu^{\circ\,'\,''}$ [DMS→] [=] Δx [STO] [x⇄y] $\Delta y + Y_S = Y_1$
[M] [+] X_S [=] X_1 (OUT)

Commodore

4190/5190
Δx [x⇄y] Δy [→P] d [x⇄y] ν^{dec} (F(d) DMS)

d [x⇄y] ν°_{DMS} ν'_{DMS} ν''_{DMS} [F INV (d) DMS] [→R] Δx [x⇄y] Δy

6120, 6140, 9120, 9140
Δx [F x⇄y] Δy [→P] d [F x⇄y] ν^{dec}

d [F x⇄y] [→R] Δx [F x⇄y] Δy

SHARP EL 506

Δx [2nd F ↕] Δy [2nd F r Θ] ⇒ d [2nd F ↕] ⇒ ν^{dec} [2nd F →DMS]

d [2nd F ↕] $\nu^{\circ\,'\,''}$ [2nd F →DEG] [2nd F →XY] ⇒ Δx [2nd F ↕] Δy

$Y_n - Y_S = [X \to M](X_0 - X_S)$ [2nd F ↕] RM [2nd F r Θ] ⇒ d [2nd F] ν^{dec} (+360°) [2nd F →DMS]

TECHNICO

Δx [+] Δy [r Θ] ⇒ d [x⇄y] ⇒ ν^{dec} [F DMS]

d [+] $\nu^{\circ\,'\,''}$ [DEG] [F →XY] ⇒ Δx [x⇄y] Δy

CANON CARD F63

Δx $\boxed{RV}$ Δy $\boxed{P \leftarrow R}$ $\Rightarrow d$ $\boxed{RV}$ $\Rightarrow \nu^{dec}$ $\boxed{a^{\circ\,'\,''} \leftarrow}$ $\quad$ d $\boxed{RV}$ $\nu^{\circ\,'\,''}$ $\boxed{a^{\circ\,'\,''} \rightarrow}$ $\boxed{P \rightarrow R}$ $\Rightarrow \Delta x$ $\boxed{RV}$ $\Rightarrow \Delta y$

CANON F 62

Δx $\boxed{\begin{matrix}INV\\R \rightarrow P\end{matrix}}$ Δy $\boxed{=}$ d $\boxed{RV}$ $\Rightarrow \nu^{dec}$ $\boxed{INV\ \alpha^{\circ\,'\,''} \leftarrow}$ $\quad$ d $\boxed{\begin{matrix}INV\\P \rightarrow R\end{matrix}}$ $\nu^{\circ\,'\,''}$ $\boxed{\alpha^{\circ\,'\,''} \rightarrow}$ $\boxed{=}$ Δx $\boxed{RV}$ Δy

MBO 4000 α

Δx $\boxed{\begin{matrix}INV\\R \rightarrow P\end{matrix}}$ Δy $\boxed{=}$ d $\boxed{x \leftrightarrow y}$ $\Rightarrow \nu^{dec}$ $\quad$ d $\boxed{\begin{matrix}INV\\P \rightarrow R\end{matrix}}$ $\nu^{\circ\,'\,''}$ $\boxed{DMS \rightarrow}$ $\boxed{=}$ Δx $\boxed{x \leftrightarrow y}$ Δy

TOSHIBA SLC 8200

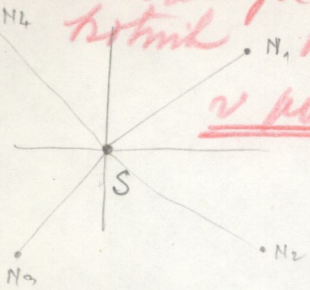
Δx $x \leftrightarrow y$ Δy $\rightarrow R\theta$ $\rightarrow d$ $x \leftrightarrow y$ ν^{dec} $\quad$ d $x \leftrightarrow y$ ν^{dec} $F \rightarrow xy$ $\Rightarrow \Delta x$ $x \leftrightarrow y$ Δy

MBO Alpha 802

$\Delta x + \Delta y$ $F\ r\ \oplus \Rightarrow \underline{r}$ $x \leftrightarrow y \rightarrow \underline{\oplus}$ $\quad$ $r * \oplus$ $F \rightarrow xy$ $\Rightarrow \underline{\Delta x}$ $x \leftrightarrow y$ $\underline{\Delta y}$

H. PACKARD (igrici)

Pretvorba pravokotnih koord. v polarne



MODE 4 EXE

za eno točko in enega stojišča

SHIFT POL($(X_n - X_s)$ SHIFT, $(Y_N - Y_s)$) EXE ⇒ d_{SN}

ALPHA J EXE ⇒ $\nu^{\circ dec}$ SHIFT $\overset{\leftarrow}{\circ\,'\,''}$ ⇒ $\nu^{\circ\,'\,''}$

za več točk in enega stojišča

MODE 4 EXE

→ X_s → ALPHA A EXE Y_s → ALPHA B EXE

→ SHIFT POL((X_n − ALPHA A) SHIFT, (Y_n − ALPHA B)) EXE ..... d

→ ALPHA J EXE --- $\nu^{\circ dec}$ SHIFT $\overset{\leftarrow}{\circ\,'\,''}$ ..... $\nu^{\circ\,'\,''}$

da ← istoležnica? → MC

Pretvorba polarnih koordinat v pravokotne

MODE 4 EXE (če se nismo v tem načinu)

za eno točko in enega stojišča

SHIFT REC(d SHIFT, ($\nu^{\circ}\,'\,''$)) EXE ... $\Delta X + X_s$ EXE ... X_N

ALPHA J EXE − $\Delta Y + Y_s$ EXE ... Y_N

za več točk in enega stojišča

MODE 4 EXE

→ X_s → ALPHA A EXE Y_s → ALPHA B EXE

→ SHIFT REC(d_n SHIFT, ($\nu_n^{\circ}\,'\,''$)) EXE .. ΔX_n + ALPHA A EXE ... X_N

→ ALPHA J EXE ... ΔY_n + ALPHA B EXE ... Y_N

prikaži tudi brez oklepaja! morda bo šlo.

da ← istoležnica? → ne

DRUŠTVO UPOKOJENCEV KODELJEVO

Ljubljana, 27.10.1987

VSEM ČLANOM IZVRŠILNEGA ODBORA DU - KODELJEVO

Vabim na sejo Izvršilnega odbora društva Kodeljevo, ki bo

v sredo 4. novembra 1987 ob 16. uri v prostorih društva upokojencev Kodeljevo Ob Ljubljanici 36 a.

Dnevni red:

1. Pregled programa dela društva upokojencev do novembra 1987.
2. Obravnava sklepa sveta KS Kodeljevo glede prostorov.

Pod tč. 1 predlagam, da bi predsedniki posameznih komisij poročali koliko je opravljenega dela po programu dela društva upokojencev za leto 1987.

Pod tč. 2. V prilogi dostavljam sklep KS Kodeljevo glede poslovnih prostorov.

Vse člane Izvršilnega odbora naprošam, da se udeležijo seje in morebitno odsotnost sporočite tajniku društva.

S tovariškim pozdravom!

URBIČ Tone

DANO: $d_{AB}^{B} = 662.844$ $\quad y_A = 956.72$

$\nu_A^B = 307°41'34''$ $\quad x_A = 316.17$

IŠČEM: y_B, x_B

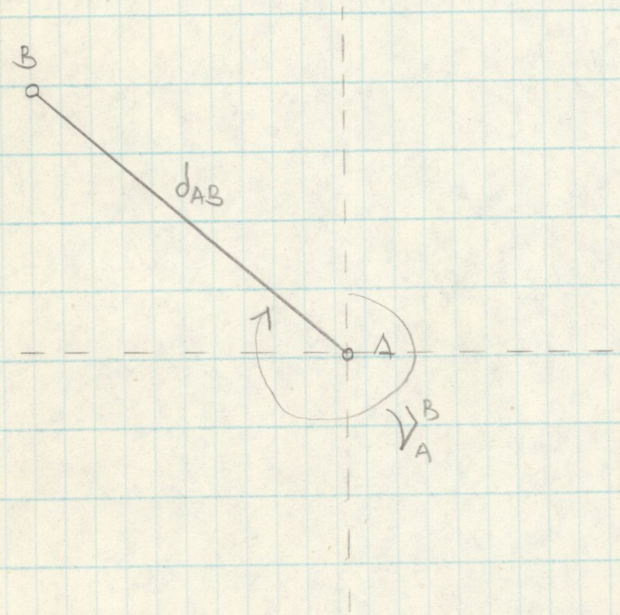
$(d_{AB}^{B}, \nu_A^{B\,°DEC}) - P \to R$

$+ x_A = \underline{721.4509} = x_B$

$+ y_A = \underline{432.21113} = y_B$

TIPKAM	SKLAD:
662.844	1: 662.844
307.4134	2: 662.844 1: 307.4134
HMS →	2: 662.844 1: 307.692777...
R→C	(662.844, 307.69277)
P→R	1: (405.2809, -524.508)
(316.17, 956.72)	2: (405.2809, -524.508) 1: (316.17, 956.72)
+	(721.4509, 432.2111)

HEWLETT PACKARD 28C



T	Y	X
A	956·72	316·17
B	432·21	721·45

POT II:

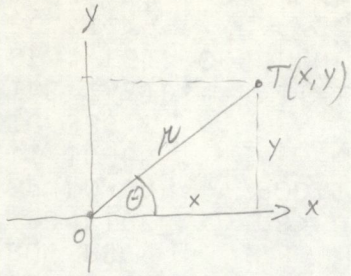
PREKO KOMPLEKSNIH ŠTEVIL, X OZ. Y OSTANE V SKLADU NA II. MESTU.

Postopek N° 1:

TIPKAM	DISPLAY
Y_B 432·21 <ENT>	1: 432·21
Y_A 956·72 <->	1: -524·51
∠	2: -524·51
721·45 <ENT>	1: 721·45
	2: -524·51
316·17 <->	1 405.28
	2: 405·28
SWAP	1: -524·51
R→C REAL → COMPLEX	1: (405·28, -524·51)
R→P REAL → POLAR	1: (662·844.., -52·307..)
C→R	2: 662·844 1: -52·307
360 <+>	2: 662·844 1: 307·603 → HMS : 307° 41' 33·5"

MIHA KRALJ

Vastwood KL-5200



$x = r \cos\theta$ $\quad r = \sqrt{x^2 + y^2}$

$y = r \sin\theta$ $\quad \theta = \arctan \frac{y}{x}$

DANO: x, y (12, 5)

$\underline{\underline{R \to P}}$

12	12	
INV R→P	12	12
5	5	12
=	13	$\boxed{22.619..}$ $\underline{\underline{r}}$
x⇄y	22.619..	$\underline{\underline{\theta}}$

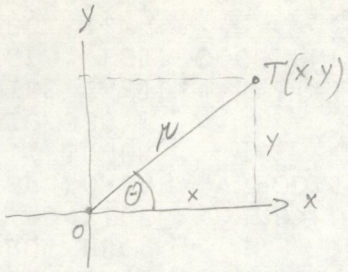
DANO $r = 36$

$\theta = 50^\circ$

$\underline{\underline{P \to R}}$

36	36	
INV P→R	36	36
50	50	36
=	23.14..	27.57..
	x	y
x⇄y	27.57	23.14
	y	x

Vastwood KL-5200



$x = r\cos\theta$ $\quad r = \sqrt{x^2+y^2}$

$y = r\sin\theta$ $\quad \theta = \arctan\frac{y}{x}$

DANO: x, y (12, 5)

$\underline{\underline{R \to P}}$

12	12	
INV R→P	12	12
	x	y
5	5	12
=	13	$\boxed{22.619..}$ $\underline{\underline{r}}$
x⇄y	22.619..	θ

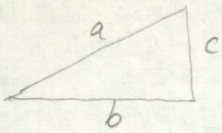
DANO $r = 36$

$\theta = 50^\circ$

$\underline{\underline{P \to R}}$

36	36	
INV P→R	36	36
50	50	36
=	23.14..	27.57..
	x	y
x⇄y	27.57	23.14
	y	x

Pitagora



$a^2 = b^2 + c^2$

$b = 5$

$c = 7$

$a = \sqrt{b^2 + c^2} = 8,602$

5	5	0
INV x^2	25	0
+	25	25 +
7	7	25 +
x^2	49	25 +
=	74	49
$\sqrt{}$	8,602	49

Kugla

Površina $F = 4\pi r^2 = 1809.56$

$V = \frac{4\pi r^3}{3} = 7238,23$

$r = 12$

4	4	
×	4	4 ×
INV π	3.14..	4 ×
×	12.57..	12.57 ×
r	12	12.57 ×
INV x^2	144	12.57 ×
=	1809.56	12.57

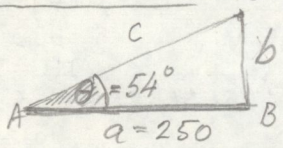
F

4		
÷		
3		
×		
INV π	3.1415	1.333333
×	4.188..	4.188 ×
(	4.188	0	4.188 ×
12	12	0	4.188 ×
x^y	12	12 y^x	4.188 ×
3	3	12 y^x	4.188 ×
)	1728	4188 ×	
=	7238,229	1728	

V

Razreševanje pravokotnika

Dano: Θ in kateta c

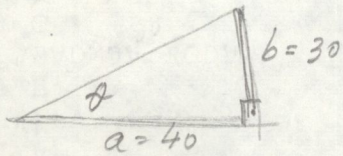


250	250	
÷	250	250 ÷
54	54	250 ÷
cos	0,59	250 ÷
=	425,33	0,59 c

$c = \frac{a}{\cos\Theta}$

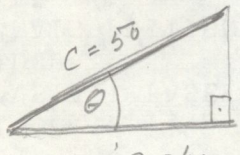
$b = a \operatorname{tg}\Theta$

250	250	
×	250	250 ×
54	54	250 ×
tan	1.376..	250 ×
=	344.095	250 b



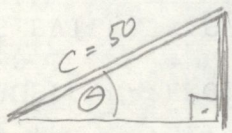
$\Theta = \operatorname{arc\,tan} \frac{b}{a}$

30	30	0
÷	30	30 ÷
40	40	30 ÷
=	0.75	30 ÷
$\tan^{-1}$	36.86989	INV ° ' " 36°52'12"



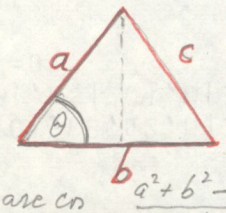
$\Theta = \operatorname{arc\,cos} \frac{a}{c}$

40		
÷		
50		
=		
$\cos^{-1}$	36.86989	" "



$\Theta = \operatorname{arc\,sin} \frac{b}{c}$

30		
÷		
50		
=		
$\sin^{-1}$	36.86989	" "



Dano $a = 6$, $b = 7$, $c = 8$ cm

Iščemo: Θ,

$\Theta = \arccos \frac{a^2 + b^2 - c^2}{2ab}$

$\Theta = 75°31'21''$

$\Theta = 75.5225$

	x	y
6		
INV x^2	6	
	36	
+	36	36 +
7	7	36 +
INV x^2	49	36 +
−	85	85 −
8	8	85 −
INV x^2	64	85 −
÷	21	21 ÷
2	2	21 ÷
÷	10.5	10.5 ÷
6	6	10.5 ÷
÷	1.75	1.75 ÷
7	7	1.75 ÷
=	6,25	7

	x	y
INV $\cos^{-1}$	75.5225	7
INV ° ' "	75°31'21"	7
° ' "	75.5225	7
sin	0.968245	7
×	0.968245	0.968245 ×
6	6	— " — ×
×	5,80947	5,80947 ×
7	7	— " — ×
÷	40,666	40.666 ÷
2	2	40.666 ÷
=	20,333	2

$P = \frac{b \cdot a \sin\Theta}{2} = 20,333\,cm^2$

```
10 COM P$[20],R8,T2,U[30]
20 DIM A$[3],E$[20],D[30],E[30],F[30]
30 D9=E9=F9=0
40 MAT D=ZER
50 MAT E=ZER
60 MAT F=ZER
70 DISP "POSLOVNA ENOTA";
80 INPUT E$
90 DISP "STEVILKA KASETE PODATKOV";
100 INPUT A
110 REWIND
120 WAIT 1000
130 DISP "VSTAVI KASETO PODATKOV"
140 WAIT 1000
150 DISP "NATO PRITISNI´1´IN´EXECUTE´";
160 INPUT A2
170 DISP "PRVA KODA";
180 INPUT B
190 DISP "ZADNJA KODA";
200 INPUT C
210 MAT U=ZER
220 LOAD  DATA 0
230 IF VAL(P$)=A THEN 270
240 DISP "NAPACNA KASETA S PODATKI"
250 WAIT 1000
260 GOTO 130
270 FOR X=B TO C
280 LOAD  DATA X
290 IF E$="RACUNOVODSTVO" THEN 320
300 IF E$=P$ THEN 320
310 GOTO 390
320 GOTO T2 OF 390,390,390,390,330,350,370
330 MAT D=D+U
340 GOTO 390
350 MAT E=E+U
360 GOTO 390
370 MAT F=F+U
380 GOTO 390
390 NEXT X
400 DISP "ALI JE OBDELAVA KONCANA";
410 INPUT A$
420 IF A$="DA" THEN 460
430 DISP "STEVILKA NASLEDNJE KASETE";
440 INPUT A
450 GOTO 110
460 S1=0
470 PRINT
480 PRINT
490 PRINT
500 PRINT
510 PRINT TAB10;"Poslovna enota:";E$
520 PRINT TAB10;"Rekapitulacija ucinkov;za ostale namene"
530 PRINT
540 PRINT
550 PRINT TAB35;"STOPNJA UCINKA"
560 PRINT "          LETO        11.50442        11.50442        13              SKUPAJ"
570 PRINT
580 FOR X=1 TO 30
590 IF D[X]+E[X]+F[X]=0 THEN 680
600 S=D[X]+E[X]+F[X]
```

Vastwood KL-5200

Faktoriel

$4! = 4.3.2.1 = 24$ 4 [INV X!]

$5! = 5.4.3.2.1 = 120$ 5 [INV X!]

Dělo s konstantami

$10 + 3 = \underline{13}$

$-4.5 + 3 = \underline{-1.5}$

$0.05 + 3 = \underline{3.05}$

10	10	
+	10	10 +
3	3	10 +
=	13	+3
4.5	4.5	3
+/-	-4.5	3
=	-1.5	+3
.05	0.05	3
=	3.05	+3

$100 - 4 = \underline{96}$

$4.5 - 4 = \underline{-8.5}$

$3.2 - 4 = \underline{-0.8}$

100	100	
-	100	100 -
4	4	100 -
=	96	-4
4.5	4.5	-4
+/-	-4.5	-4
=	-8.5	-4
3,2	3.2	-4
=	-0.8	-4

$100 \div [(45+53) \times (23-35) + 50] = 0.0888099467$

$5 \times 6 = 30$

$5 \times 9 = 45$

$5 \times 2 = 10$

5	5	0
x	5	5x
6	6	5x
=	30	5
9	9	5x
=	45	5x
2	2	5x
=	10	5

```
650 F9=F[X]+F9
660 FORMAT 5X,F5.0,2X,4F13.2
670 NEXT X
680 PRINT "      ------------------------------------------------------------"
690 WRITE (15,660)0,D9,E9,F9,S1
700 REWIND
710 FORMAT B
720 WRITE (15,710)12
730 END
```